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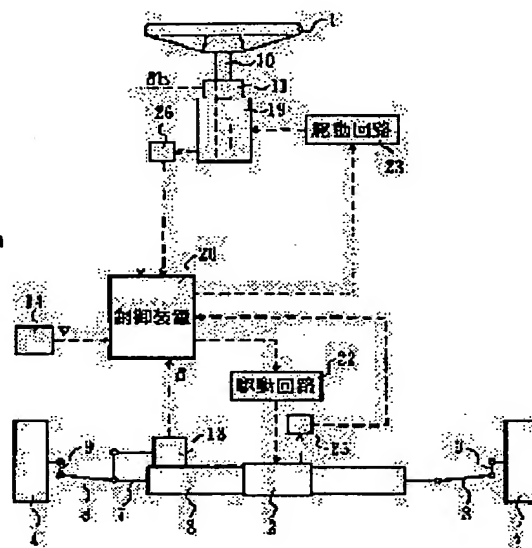
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## (54) STEERING DEVICE FOR VEHICLE

## (57)Abstract:

**PROBLEM TO BE SOLVED:** To provide a steering device for a vehicle capable of preventing a reduction of steering performance without imparting a sense of incompatibility to a driver when an upper limit value of an output of a steering actuator is restricted in order to prevent an excessive loading in a vehicle adopting a steer-by-wire system.

**SOLUTION:** A steering angle is varied corresponding to a motion of the steering actuator 2 driven in responsive to a rotation of an operation member 1 without mechanically connecting the operation member 1 to wheels 4. A degree of generated reflection force of an operation actuator 19 for acting to a direction returning the operation member 1 to a straight advancement position is made large when a restriction degree of the output of the steering actuator 2 according to a restriction condition previously set becomes large.



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CLAIMS

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[Claim(s)]

[Claim 1] Without connecting the operating member with an operating member and the actuator for steering driven according to the revolution of the operating member mechanically at a wheel, so that a rudder angle may change according to a motion of the actuator for steering The device in which the motion is transmitted to a wheel, and a means to restrict the upper limit of the output of the actuator for steering according to the restriction set up beforehand, The actuator for actuation which can generate the reaction force which acts in the direction which returns the operating member to a rectilinear-propagation location, Based on a means to memorize the response relation defined beforehand and its response relation between limit extent and the magnitude of reaction force of the upper limit of the output of the actuator for steering, so that the magnitude of reaction force may change according to the limit extent The power steering system of a car equipped with a means to control the actuator for actuation.

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## DETAILED DESCRIPTION

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[Detailed Description of the Invention]

[0001]

[Field of the Invention] This invention relates to the power steering system of the car which adopted the so-called steer BAIWAIYA system.

[0002]

[Description of the Prior Art] In the car which adopted the steer BAIWAIYA system, the motion of the actuator for steering driven according to the revolution of the operating member is delivered that a rudder angle changes according to the motion to the wheel, without connecting with a wheel mechanically the operating member which imitated the steering wheel. Therefore, the steering resistance or the self-aligning torque based on friction between a wheel and a road surface are not transmitted to the operating member.

[0003] Then, by forming the actuator for actuation on which the reaction force of the direction which returns the operating member to a rectilinear-propagation location is made to act, like the usual car with which the steering wheel was mechanically connected with the wheel, a steering feeling is given to a driver and the operating member is returned to the rectilinear-propagation location.

[0004]

[Problem(s) to be Solved by the Invention] In the car which adopted the steer BAIWAIYA system, when setting, performing end steering continuously or performing slalom transit and sudden steering frequently, the load of the actuator for steering increases and the calorific value of electronic parts, such as a switching element for power control of the actuator for steering, increases. Then, like the cure against overload protection of the motor for steering auxiliary force generating in the electric power-steering equipment of the usual car, if the variate corresponding to loads, such as continuation actuation time amount of the actuator for steering and an integrated value of an energization current, results in the set point, it is possible to restrict the upper limit of the output of the actuator for steering.

[0005] However, in the car which adopted the steer BAIWAIYA system, even if it restricts the output of the actuator for steering for overload protection, since the wheel and the operating member are not connected mechanically, actuation of an operating member is not restricted. Therefore, the responsibility of rudder angle change of the car to actuation of an operating member falls, smooth steering cannot be performed but the controllability ability of a car falls. Moreover, since it is difficult for a driver to grasp the load limitation of the actuator for steering which is the cause of lowering of the responsibility, a driver senses sense of incongruity.

[0006]

[Means for Solving the Problem] The actuator for steering which drives the power steering system of the car of this invention according to the revolution of an operating member and its operating member, Without connecting the operating member with a wheel mechanically, so that a rudder angle may change according to a motion of the actuator for steering The device in which the motion is transmitted to a wheel, and a means to restrict the upper limit of the output of the actuator for steering according to the restriction set up beforehand, The actuator for actuation which can generate the reaction force which acts in the direction which returns the operating member to a rectilinear-propagation location, It has a means to memorize the response relation as which it was beforehand determined between limit extent and the magnitude of reaction force of the upper limit of the output of the actuator for steering, and a means to

control the actuator for actuation so that the magnitude of reaction force changes according to the limit extent based on the response relation. Since according to the configuration of this invention the generating reaction force of the actuator for actuation becomes large when the upper limit of the output of the actuator for steering is restricted for overload protection, it can prevent that the responsibility of rudder angle change of the wheel to actuation of an operating member falls.

[0007]

[Embodiment of the Invention] The operating member 1 in which the power steering system of the car shown in drawing 1 imitated the steering wheel, Without connecting the operating member 1 with the actuator 2 for steering driven according to the revolution of the operating member 1 mechanically at a wheel 4, so that a rudder angle may change according to a motion of the actuator 2 for steering It has the steering gear 3 which transmit the motion to a wheel 4, and the actuator 19 for actuation which can generate the reaction force which acts in the direction which returns the operating member 1 to a rectilinear-propagation location.

[0008] Electric motors, such as a well-known brushless motor, can constitute the actuator 2 for steering, for example. The steering gear 3 are constituted by motion translators, such as for example, a ball screw device in which rotation of the power shaft of the actuator 2 for steering is changed into the rectilinear motion of the steering rod 7. A motion of the steering rod 7 is transmitted to a wheel 4 through a tie rod 8 and a steering knuckle arm 9, and the toe angle of the wheel 4 changes. A well-known thing can be used for the steering gear 3, and a configuration will not be limited if a motion of the actuator 2 for steering can be delivered that a rudder angle changes to a wheel 4. In addition, in the condition that the actuator 2 for steering is not driving, the wheel alignment is set up so that a wheel 4 can return to a rectilinear-propagation location by the self-aligning torque.

[0009] The operating member 1 is connected with the revolution shaft 10 supported by the car-body side pivotable. The power shaft of the actuator 19 for actuation is united with the revolution shaft 10. Electric motors, such as a brushless motor, can constitute the actuator 19 for actuation.

[0010] As a means to calculate the rotation from the rectilinear-propagation location of the operating member 1, the angle sensor 11 which detects angle-of-rotation  $\Delta\theta$  from the rectilinear-propagation location of the operating member 1 is formed. The rudder angle sensor 13 constituted as a means to detect the rudder angle  $\Delta\delta$  of a car by the potentiometer which detects the travel of the steering rod 7 is formed. The rate sensor 14 which detects the vehicle speed  $V$  is formed. The angle sensor 11, the rudder angle sensor 13, and the rate sensor 14 are connected to the control unit 20 constituted by computer. Moreover, the current detection sensor 25 which detects the current value of the actuator 2 for steering, and the current detection sensor 26 which detects the current value of the actuator 19 for actuation are connected to the control device 20.

[0011] The control device 20 controls the actuator 2 for steering through the actuation circuit 22. For example, the relation between angle-of-rotation  $\Delta\theta$  of the operating member 1, and the vehicle speed  $V$  and a target rudder angle is defined beforehand, and is memorized, and the driving signal of the actuator 2 for steering is outputted through the actuation circuit 22 so that the deflection of the target rudder angle and the detected rudder angle  $\Delta\delta$  may be lost. The relation between the angle-of-rotation  $\Delta\theta$ , and the vehicle speed  $V$  and a target rudder angle can plan improvement in the turnability in a low speed, and transit stability in a high speed by making small the target rudder angle corresponding to angle-of-rotation  $\Delta\theta$ , so that the vehicle speed  $V$  becomes large. In addition, especially the control approach of such an actuator 2 for steering is not limited. That what is necessary is just what the actuator 2 for steering drives according to the revolution of an operating member 1 For example, the yaw rate sensor of a car may be prepared, the relation between angle-of-rotation  $\Delta\theta$  of an operating member 1 and a target yaw rate may be defined beforehand, and may be memorized, and the driving signal of the actuator 2 for steering may be outputted through the actuation circuit 22 so that the deflection of a detection yaw rate and a target yaw rate may be lost.

[0012] The control device 20 memorizes the restriction which the upper limit of the output of the actuator 2 for steering set up beforehand, and restricts the upper limit of the output of the actuator 2 for steering according to the restriction. The restriction shall be satisfied if the variate corresponding to the load of the actuator 2 for steering results in the set point. With this

operation gestalt, a control unit 20 calculates the integrated value of the energization current of the actuator 2 for steering based on the detection value of the current detection sensor 25 as a variate corresponding to the load. As shown in drawing 2, when a restriction is satisfied very much by the 1st set point e which the integrated value defined beforehand, reducing the upper limit of the indicator current corresponding to the output of the actuator 2 for steering from Maximum  $I_{max}$  to the minimum value  $I_{min}$  is started, and the relation of the upper limit and integrated value is memorized by the control unit 20. When the integrated value results in the 2nd set point f defined beforehand, the upper limit shall be the minimum value  $I_{min}$ .

[0013] The control unit 20 memorizes the relation shown in drawing 3 as response relation as which it was beforehand determined between angle-of-rotation  $\delta\theta$  from the car rectilinear-propagation location of an operating member 1, and the magnitude of reaction force. The drawing 3 is target current  $I^*$  of the actuator 19 for actuation corresponding to the angle-of-rotation  $\delta\theta$  and reaction force. An example of relation is shown. Angle-of-rotation  $\delta\theta$  and target current  $I^*$  When an operating member 1 is located in the method of left [ location / rectilinear-propagation ] Uichi, forward, When located in right-and-left another side, in order to consider as negative and to secure the play of an operating member 1 [ near the rectilinear-propagation location ], the magnitude of angle-of-rotation  $\delta\theta$  is target current  $I^*$  below in the set point (the example of a graphic display 10 degrees). It is made zero. When the set point is exceeded, it is target current  $I^*$  to the change in the magnitude of angle-of-rotation  $\delta\theta$ . It shall fluctuate proportionally. The angle-of-rotation  $\delta\theta$  and target current  $I^*$  which were memorized By controlling the actuator 19 for actuation by the control device 20 based on the response relation of a between, the reaction force corresponding to angle-of-rotation  $\delta\theta$  for which it asked occurs.

[0014] The control device 20 memorizes the response relation as which it was beforehand determined between limit extent of the upper limit of the output of the actuator 2 for steering, and the magnitude of the reaction force generated with the above-mentioned actuator 19 for actuation, and based on the response relation, it controls the actuator 19 for actuation so that the magnitude of reaction force changes according to the limit extent. For example, the condition, i.e., the upper limit, that the output of the actuator 2 for steering is not restricted is Maximum  $I_{max}$ , and according to the relation shown as a continuous line E in drawing 3, the reaction force according to angle-of-rotation  $\delta\theta$  occurs until the integrated value of the energization current of the actuator 2 for steering results in the 1st set point e in drawing 2. Moreover, the integrated value of the energization current of the actuator 2 for steering results in the 2nd set point f, and when the upper limit is the minimum value  $I_{min}$  According to the relation shown with a two-dot chain line F in drawing 3, the reaction force according to angle-of-rotation  $\delta\theta$  occurs. When it is a value in the middle of making it increase from the middle of the upper limit decreasing from Maximum  $I_{max}$  to the minimum value  $I_{min}$ , or the minimum value  $I_{min}$  to Maximum  $I_{max}$  According to the relation shown with an alternate long and short dash line G in drawing 3 defined according to the value, the reaction force according to angle-of-rotation  $\delta\theta$  shall be generated. Target current  $I^*$  to angle-of-rotation  $\delta\theta$  of an operating member 1, so that limit extent of the upper limit of the indicator current corresponding to the output of the actuator 2 for steering by this is large An increment rate becomes large and reaction force is enlarged. Namely, angle-of-rotation  $\delta\theta$  of an operating member 1 and target current  $I^*$  of the actuator 19 for actuation according to a upper limit A control unit 20 memorizes the relation of a between.

[0015] The control procedure of the actuator 19 for actuation by the above-mentioned control device 20 is explained with reference to the flow chart of drawing 4. First, target current  $I^*$  of the actuator 19 for actuation corresponding to [ read angle-of-rotation  $\delta\theta$  of an operating member 1, and the value of the energization current  $I$  of the actuator 19 for actuation detected by the current detection sensor 26 (step 101), and ] the angle-of-rotation  $\delta\theta$  and the upper limit of the indicator current of the actuator 2 for steering Target current  $I^*$  according to the angle-of-rotation  $\delta\theta$  and upper limit It calculates based on the relation which between memorized (step 102). The target current  $I^*$  The driving signal of the actuator 19 for actuation is outputted through the actuation circuit 23 so that deflection with the energization current  $I$  of the actuator 19 for actuation may be lost (step 103), and it returns to step 101.

[0016] According to the above-mentioned configuration, when the upper limit of the output of the actuator 2 for steering is restricted for overload protection, the generating reaction force of

the actuator 19 for actuation becomes large. Moreover, the generating reaction force of the actuator 19 for actuation becomes large, so that the upper limit of the output of the actuator 2 for steering is restricted. Thereby, when the upper limit of the output of the actuator 2 for steering is restricted, it can prevent that the responsibility of the rudder angle change to actuation of an operating member 1 falls.

[0017] This invention is not limited to the above-mentioned operation gestalt. For example, the magnitude of reaction force may not be limited to what changes according to angle of rotation of an operating member, you may change according to other service conditions of the rotational speed and roll acceleration of an operating member, and the reaction force may be fixed. Furthermore, it is made to make the return resistance force which acts on the direction which returns not only reaction force but an operating member to a rectilinear-propagation location with the actuator for actuation, and an opposite direction act, and the magnitude of the return resistance force may be made equivalent to limit extent of the upper limit of the output of the actuator for steering, and may be changed. Moreover, it may be made for the restriction of the upper limit of the output of the actuator for steering to reduce the upper limit by whenever [ undermoderation / which was set up that what is necessary is just what is set to be able to prevent the overload of the actuator for steering when the continuation actuation time amount of the actuator for steering became the set point ], and you may make it ease a restriction, so that the ambient temperature of the actuator for steering detected with the temperature sensor is low.

[0018]

[Effect of the Invention] When restricting the upper limit of the output of the actuator for steering in the car which adopted the steer BAWAIYA system for overload protection according to this invention, the power steering system of the car which can prevent that controllability ability falls can be offered without a driver sensing sense of incongruity.

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## DESCRIPTION OF DRAWINGS

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### [Brief Description of the Drawings]

[Drawing 1] The configuration explanatory view of the power steering system of the car of the operation gestalt of this invention

[Drawing 2] Drawing showing an example of the relation of the energization current integrated value of the actuator for steering and indicator current upper limit in the power steering system of the car of the operation gestalt of this invention

[Drawing 3] Drawing showing an example of the relation of the angle of rotation of an operating member and the target current of the actuator for actuation in the power steering system of the car of the operation gestalt of this invention

[Drawing 4] The flow chart which shows the control procedure of the actuator for actuation in the power steering system of the car of the operation gestalt of this invention

### [Description of Notations]

1 Operating Member

2 Actuator for Steering

3 Steering Gear

4 Wheel

19 Actuator for Actuation

20 Control Unit

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(2)

## 【特許請求の範囲】

【請求項 1】 操作部材と、その操作部材の回転に応じて駆動される操舵用アクチュエータと、その操作部材を車輪に機械的に連結することなく、その操舵用アクチュエータの動きに応じて舵角が変化するように、その動きを車輪に伝達する機構と、その操舵用アクチュエータの出力の上限値を、予め設定した制限条件に従って制限する手段と、その操作部材を直進位置に復帰させる方向に作用する反力を発生可能な操作用アクチュエータと、その操舵用アクチュエータの出力の上限値の制限程度と、その反力の大きさととの間の予め定められた対応関係を記憶する手段と、その対応関係に基づき、その制限程度に応じて反力の大きさが変化するように、その操作用アクチュエータを制御する手段とを備える車両の操舵装置。

## 【発明の詳細な説明】

【0001】

【発明の属する技術分野】 本発明は、いわゆるステアバイワイヤシステムを採用した車両の操舵装置に関する。

【0002】

【従来の技術】 ステアバイワイヤシステムを採用した車両においては、ステアリングホイールを模した操作部材を車輪に機械的に連結することなく、その操作部材の回転に応じて駆動される操舵用アクチュエータの動きを、その動きに応じて舵角が変化するように車輪に伝達している。そのため、車輪と路面との間の摩擦に基づく操舵抵抗やセルフアライニングトルクは、その操作部材には伝達されない。

【0003】 そこで、その操作部材を直進位置に戻す方向の反力を作用させる操作用アクチュエータを設けることで、ステアリングホイールが車輪に機械的に連結された通常の車両と同様に、ドライバーに操舵フィーリングを与え、また、操作部材を直進位置に復帰させている。

【0004】

【発明が解決しようとする課題】 ステアバイワイヤシステムを採用した車両において、据え切り操舵を連続して行ったり、スラローム走行や急操舵を頻繁に行う場合、操舵用アクチュエータの負荷が増大し、また、操舵用アクチュエータの電力制御用スイッチング素子等の電子部品の発熱量が増大する。そこで、通常の車両の電動パワーステアリング装置における操舵補助力発生用モータの過負荷防止対策と同様に、操舵用アクチュエータの連続駆動時間や通電電流の積算値等の負荷に対応する変量が設定値に至ったならば、その操舵用アクチュエータの出力の上限値を制限することが考えられる。

【0005】 しかし、ステアバイワイヤシステムを採用した車両においては、操舵用アクチュエータの出力を過負荷防止のために制限しても、車輪と操作部材とは機械的に連結されていないので、操作部材の操作は制限されない。そのため、操作部材の操作に対する車両の舵角変化の応答性が低下し、円滑な操舵を行うことができず車

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両の操縦性能が低下する。また、その応答性の低下原因である操舵用アクチュエータの出力制限をドライバーが把握するのは困難であるため、ドライバーは違和感を感じる。

【0006】

【課題を解決するための手段】 本発明の車両の操舵装置は、操作部材と、その操作部材の回転に応じて駆動される操舵用アクチュエータと、その操作部材を車輪に機械的に連結することなく、その操舵用アクチュエータの動きに応じて舵角が変化するように、その動きを車輪に伝達する機構と、その操舵用アクチュエータの出力の上限値を、予め設定した制限条件に従って制限する手段と、その操作部材を直進位置に復帰させる方向に作用する反力を発生可能な操作用アクチュエータと、その操舵用アクチュエータの出力の上限値の制限程度と、その反力の大きさととの間の予め定められた対応関係を記憶する手段と、その対応関係に基づき、その制限程度に応じて反力の大きさが変化するように、その操作用アクチュエータを制御する手段とを備える。本発明の構成によれば、過負荷防止のために操舵用アクチュエータの出力の上限値が制限される時、操作用アクチュエータの発生反力が大きくなるので、操作部材の操作に対する車輪の舵角変化の応答性が低下するのを防止できる。

【0007】

【発明の実施の形態】 図 1 に示す車両の操舵装置は、ステアリングホイールを模した操作部材 1 と、その操作部材 1 の回転に応じて駆動される操舵用アクチュエータ 2 と、その操作部材 1 を車輪 4 に機械的に連結することなく、その操舵用アクチュエータ 2 の動きに応じて舵角が変化するように、その動きを車輪 4 に伝達するステアリングギヤ 3 と、その操作部材 1 を直進位置に復帰させる方向に作用する反力を発生可能な操作用アクチュエータ 19 とを備える。

【0008】 その操舵用アクチュエータ 2 は、例えば公知のブラシレスモータ等の電動モータにより構成できる。そのステアリングギヤ 3 は、その操舵用アクチュエータ 2 の出力シャフトの回転運動をステアリングロッド 7 の直線運動に変換する例えばボールねじ機構等の運動変換機構により構成されている。そのステアリングロッド 7 の動きがタイロッド 8 とナックルアーム 9 を介して車輪 4 に伝達され、その車輪 4 のトー角が変化する。そのステアリングギヤ 3 は、公知のものをを用いることができ、操舵用アクチュエータ 2 の動きを舵角が変化するように車輪 4 に伝達できれば構成は限定されない。なお、操舵用アクチュエータ 2 が駆動されていない状態では、車輪 4 はセルフアライニングトルクにより直進位置に復帰できるようにホイールアラインメントが設定されている。

【0009】 その操作部材 1 は、車体側により回転可能に支持される回転シャフト 10 に連結されている。その

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回転シャフト10に操作用アクチュエータ19の出力シャフトが一体化されている。その操作用アクチュエータ19はブラシレスモータ等の電動モータにより構成できる。

【0010】その操作部材1の直進位置からの回転量を求める手段として、その操作部材1の直進位置からの回転角度 $\delta h$ を検出する角度センサ11が設けられている。車両の舵角 $\delta$ を検出する手段として、ステアリングロッド7の作動量を検出するポテンシオメータにより構成される舵角センサ13が設けられている。車速 $V$ を検出する速度センサ14が設けられている。その角度センサ11、舵角センサ13、速度センサ14は、コンピュータにより構成される制御装置20に接続されている。また、その制御装置20に、操舵用アクチュエータ2の電流値を検出する電流検出センサ25と、操作用アクチュエータ19の電流値を検出する電流検出センサ26とが接続されている。

【0011】その制御装置20は、駆動回路22を介して操舵用アクチュエータ2を制御する。例えば、その操作部材1の回転角度 $\delta h$ と車速 $V$ と目標舵角との間の関係を予め定めて記憶し、その目標舵角と検出した舵角 $\delta$ との偏差をなくすように駆動回路22を介して操舵用アクチュエータ2の駆動信号を出力する。その回転角度 $\delta h$ と車速 $V$ と目標舵角との間の関係は、車速 $V$ が大きくなる程に回転角度 $\delta h$ に対応する目標舵角を小さくすることで、低速での旋回性能の向上と高速での走行安定性を図ることができる。なお、このような操舵用アクチュエータ2の制御方法は特に限定されず、操作部材1の回転に応じて操舵用アクチュエータ2が駆動されるものであれば良く、例えば、車両のヨーレートセンサを設け、操作部材1の回転角度 $\delta h$ と目標ヨーレートとの間の関係を予め定めて記憶し、検出ヨーレートと目標ヨーレートとの偏差をなくすように駆動回路22を介して操舵用アクチュエータ2の駆動信号を出力してもよい。

【0012】その制御装置20は、その操舵用アクチュエータ2の出力の上限値の予め設定した制限条件を記憶し、その制限条件に従って操舵用アクチュエータ2の出力の上限値を制限する。その制限条件は、操舵用アクチュエータ2の負荷に対応する変量が設定値に至ったならば充足するものとされる。本実施形態では、その負荷に対応する変量として操舵用アクチュエータ2の通電電流の積算値を電流検出センサ25の検出値に基づき制御装置20が演算する。図2に示すように、その積算値が予め定めた第1設定値 $e$ に至って制限条件が充足されることにより、操舵用アクチュエータ2の出力に対応する指示電流の上限値を最大値 $I_{max}$ から最小値 $I_{min}$ まで低減することが開始され、その上限値と積算値との関係が制御装置20に記憶される。その積算値が予め定めた第2設定値 $f$ に至った時に、その上限値は最小値 $I_{min}$ になるものとされている。

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【0013】その制御装置20は、操作部材1の車両直進位置からの回転角度 $\delta h$ と反力の大きさとの間の予め定められた対応関係として、図3に示す関係を記憶する。その図3は、その回転角度 $\delta h$ と反力に対応する操作用アクチュエータ19の目標電流 $I^*$ との関係の一例を示し、回転角度 $\delta h$ と目標電流 $I^*$ は操作部材1が直進位置よりも左右一方に位置する時は正、左右他方に位置する時は負とされ、直進位置近傍において操作部材1の遊びを確保するために回転角度 $\delta h$ の大きさが設定値（図示例では10度）以下では目標電流 $I^*$ を零にし、その設定値を超えると回転角度 $\delta h$ の大きさの増減に目標電流 $I^*$ が比例して増減するものとされている。その記憶した回転角度 $\delta h$ と目標電流 $I^*$ との間の対応関係に基づき制御装置20により操作用アクチュエータ19を制御することで、求めた回転角度 $\delta h$ に対応する反力が発生する。

【0014】その制御装置20は、その操舵用アクチュエータ2の出力の上限値の制限程度と、上記操作用アクチュエータ19により発生する反力の大きさとの間の予め定められた対応関係を記憶し、その対応関係に基づき、その制限程度に応じて反力の大きさが変化するように、その操作用アクチュエータ19を制御する。例えば、その操舵用アクチュエータ2の出力が制限されていない状態、すなわち、その上限値が最大値 $I_{max}$ であって、図2において操舵用アクチュエータ2の通電電流の積算値が第1設定値 $e$ に至るまでは、図3において実線Eで示す関係に従って回転角度 $\delta h$ に応じた反力が発生する。また、操舵用アクチュエータ2の通電電流の積算値が第2設定値 $f$ に至り、その上限値が最小値 $I_{min}$ である時は、図3において二点鎖線Fで示す関係に従って回転角度 $\delta h$ に応じた反力が発生し、その上限値が最大値 $I_{max}$ から最小値 $I_{min}$ まで低減する途中や最小値 $I_{min}$ から最大値 $I_{max}$ まで増大させる途中の値である時は、その値に応じて定められた図3において一点鎖線Gで示す関係に従って回転角度 $\delta h$ に応じた反力が発生するものとされている。これにより、その操舵用アクチュエータ2の出力に対応する指示電流の上限値の制限程度が大きい程に、操作部材1の回転角度 $\delta h$ に対する目標電流 $I^*$ の増加割合が大きくなって反力が大きくされる。すなわち、操作部材1の回転角度 $\delta h$ と、上限値に応じた操作用アクチュエータ19の目標電流 $I^*$ との間の関係を制御装置20は記憶する。

【0015】上記制御装置20による操作用アクチュエータ19の制御手順を図4のフローチャートを参照して説明する。まず、操作部材1の回転角度 $\delta h$ と、電流検出センサ26により検出した操作用アクチュエータ19の通電電流 $I$ の値を読み込み（ステップ101）、その回転角度 $\delta h$ と、操舵用アクチュエータ2の指示電流の上限値とに対応する操作用アクチュエータ19の目標電流 $I^*$ を、その回転角度 $\delta h$ と上限値に応じた目標電流

(4)

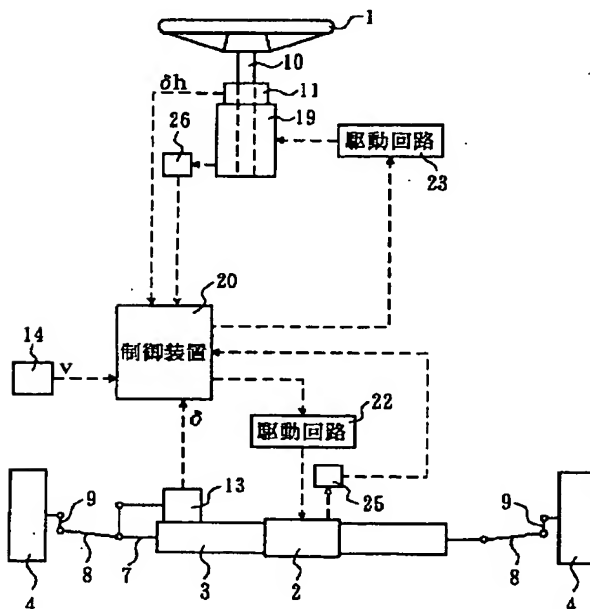
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$I^*$  との間の記憶した関係に基づき演算する（ステップ102）。その目標電流  $I^*$  と操作用アクチュエータ19の通電電流  $I$  との偏差をなくすように駆動回路23を介して操作用アクチュエータ19の駆動信号を出力し（ステップ103）、ステップ101に戻る。

【0016】上記構成によれば、過負荷防止のために操舵用アクチュエータ2の出力の上限値が制限される時、操作用アクチュエータ19の発生反力が大きくなる。また、操舵用アクチュエータ2の出力の上限値を制限する程に操作用アクチュエータ19の発生反力が大きくなる。これにより、操舵用アクチュエータ2の出力の上限値が制限される時に、操作部材1の操作に対する舵角変化の応答性が低下するのを防止できる。

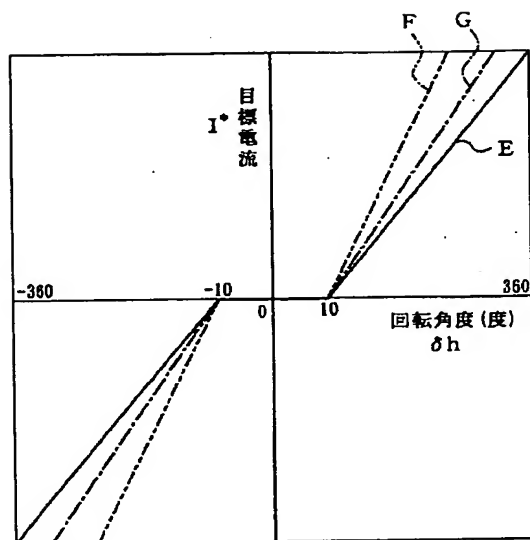
【0017】本発明は上記実施形態に限定されない。例えば、反力の大きさは操作部材の回転角度に応じて変化するものに限定されず、操作部材の回転速度や回転加速度といった他の運転条件に応じて変化してもよい、また、その反力は一定であってもよい。さらに、操作用アクチュエータにより反力だけでなく、操作部材を直進位置に復帰させる方向と反対方向に作用する復帰抵抗力を作用させるようにし、その復帰抵抗力の大きさを操舵用アクチュエータの出力の上限値の制限程度に対応させて変化させてもよい。また、操舵用アクチュエータの出力の上限値の制限条件は、操舵用アクチュエータの過負荷を防止できるように定められているものであればよく、例えば、操舵用アクチュエータの連続駆動時間が設定値になった時に設定された低減速度でその上限値を低減す

【図1】



(5)

【図3】



【図4】

